

FORM PTO-1390 (Modified) (REV 11-2000)		U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE	ATTORNEY'S DOCKET NUMBER 209326US2PCT
TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371			U.S. APPLICATION NO. (IF KNOWN, SEE 37 CFR 09/869322)
INTERNATIONAL APPLICATION NO. PCT/JP00/07926	INTERNATIONAL FILING DATE 10 November 2000	PRIORITY DATE CLAIMED 13 December 1999	
TITLE OF INVENTION PERMANENT-MAGNET MOTOR AND ITS MANUFACTURING METHOD			
APPLICANT(S) FOR DO/EO/US TAJIMA Tsuneyoshi et al.			
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:			
<ol style="list-style-type: none"> 1. <input checked="" type="checkbox"/> This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 2. <input type="checkbox"/> This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 3. <input checked="" type="checkbox"/> This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (24) indicated below. 4. <input type="checkbox"/> The US has been elected by the expiration of 19 months from the priority date (Article 31). 5. <input checked="" type="checkbox"/> A copy of the International Application as filed (35 U.S.C. 371 (c) (2)) <ol style="list-style-type: none"> a. <input type="checkbox"/> is attached hereto (required only if not communicated by the International Bureau). b. <input checked="" type="checkbox"/> has been communicated by the International Bureau. c. <input type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US). 6. <input checked="" type="checkbox"/> An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)). <ol style="list-style-type: none"> a. <input checked="" type="checkbox"/> is attached hereto. b. <input type="checkbox"/> has been previously submitted under 35 U.S.C. 154(d)(4). 7. <input checked="" type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3)) <ol style="list-style-type: none"> a. <input type="checkbox"/> are attached hereto (required only if not communicated by the International Bureau). b. <input type="checkbox"/> have been communicated by the International Bureau. c. <input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired. d. <input checked="" type="checkbox"/> have not been made and will not be made. 8. <input type="checkbox"/> An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)). 9. <input checked="" type="checkbox"/> An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)). 10. <input type="checkbox"/> An English language translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)). 11. <input type="checkbox"/> A copy of the International Preliminary Examination Report (PCT/IPEA/409). 12. <input checked="" type="checkbox"/> A copy of the International Search Report (PCT/ISA/210). <p>Items 13 to 20 below concern document(s) or information included:</p> <ol style="list-style-type: none"> 13. <input type="checkbox"/> An Information Disclosure Statement under 37 CFR 1.97 and 1.98. 14. <input type="checkbox"/> An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included. 15. <input checked="" type="checkbox"/> A FIRST preliminary amendment. 16. <input type="checkbox"/> A SECOND or SUBSEQUENT preliminary amendment. 17. <input type="checkbox"/> A substitute specification. 18. <input type="checkbox"/> A change of power of attorney and/or address letter. 19. <input type="checkbox"/> A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825. 20. <input type="checkbox"/> A second copy of the published international application under 35 U.S.C. 154(d)(4). 21. <input type="checkbox"/> A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4). 22. <input type="checkbox"/> Certificate of Mailing by Express Mail 23. <input checked="" type="checkbox"/> Other items or information: <p>Notice for Consideration of Documents Cited in International Search Report Notice of Priority/Drawings (11 Sheets)</p>			

U.S. APPLICATION NO. (IF KNOWN, SEE 37 CFR

INTERNATIONAL APPLICATION NO.

JC18 Rec'd PCT/PTO 24 JUL 2001

ATTORNEY'S DOCKET NUMBER

09/869322

PCT/JP00/07926

209326US2PCT

24. The following fees are submitted:

BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)) :**CALCULATIONS PTO USE ONLY**

- ☐ Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO \$1000.00
- ☒ International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO \$860.00
- ☐ International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO \$710.00
- ☐ International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4) \$690.00
- ☐ International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) \$100.00

ENTER APPROPRIATE BASIC FEE AMOUNT =**\$860.00**Surcharge of \$130.00 for furnishing the oath or declaration later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 CFR 1.492 (e)).**\$0.00**

CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE
Total claims	10 - 20 =	0	x \$18.00
Independent claims	3 - 3 =	0	x \$80.00

\$0.00**\$0.00**Multiple Dependent Claims (check if applicable). ☐**\$0.00****TOTAL OF ABOVE CALCULATIONS =****\$860.00**☒ Applicant claims small entity status. (See 37 CFR 1.27). The fees indicated above are reduced by 1/2.**\$0.00****SUBTOTAL =****\$860.00**Processing fee of \$130.00 for furnishing the English translation later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 CFR 1.492 (f)).**\$0.00****TOTAL NATIONAL FEE =****\$860.00**Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31) (check if applicable). ☐**\$0.00****TOTAL FEES ENCLOSED =****\$860.00**Amount to be:
refunded

\$

charged

\$

- a. ☒ A check in the amount of **\$860.00** to cover the above fees is enclosed.
- b. ☐ Please charge my Deposit Account No. _____ in the amount of _____ to cover the above fees. A duplicate copy of this sheet is enclosed.
- c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. **15-0030**. A duplicate copy of this sheet is enclosed.
- d. ☐ Fees are to be charged to a credit card. **WARNING:** Information on this form may become public. **Credit card information should not be included on this form.** Provide credit card information and authorization on PTO-2038.

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:

**22850**

Surinder Sachar
Registration No. 34,423

SIGNATURE

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NAME

24,913

REGISTRATION NUMBER

DATE

7-24-01

09/869322

JC18 Rec'd PCT/PTO 2 4 JUL 2001

209326US

IN THE UNITED STATES PATENT & TRADEMARK OFFICE

IN RE APPLICATION OF :
TSUNEYOSHI TAJIMA ET AL : ATTN: APPLICATION DIVISION
SERIAL NO: NEW U.S. PCT APPLN :
(Based on PCT/JP00/07926)
FILED: HEREWITH :
FOR: PERMANENT-MAGNET MOTOR :
AND ITS MANUFACTURING
METHOD

PRELIMINARY AMENDMENT

ASSISTANT COMMISSIONER FOR PATENTS
WASHINGTON, D.C. 20231

SIR:

Prior to a first examination on the merits, please amend the above-identified application as follows:

IN THE SPECIFICATION

Please replace the paragraph at page 8, lines 14-20, as follows:

Given a radius of an arc of the outer diameter side of the containing hole 13 provided to the rotor core 12 is R , and a radius of the outer circle of the rotor 10 is R' , it is set as $R < R'$. The arc of the outer diameter side of the containing hole 13 is set to be a part of a circumference of a circle whose center is the same to the center of the outer circle of the rotor 10. Consequently, the thickness t of the rotor core part 12a in the diameter direction has a constant value.

Please replace the paragraph at page 9, lines 10-17, as follows:

Although the magnetic orientation is set so that the focus should be located outside of the rotor 10, the residual magnetic flux density cannot be decreased. This is because the compression direction at forming the permanent magnet becomes almost the same to the direction of the magnetic flux when the cross section of the permanent magnet 14 is shaped convex to the inner diameter side, and a radius R of the convex part of the inner diameter side is set to be smaller than a radius R of the outer diameter side as shown in Fig. 1.

Please replace the paragraph at page 9, lines 18-25, as follows:

On the contrary to the case of Fig. 1, when it is desired that the radius R of the convex part of the inner diameter side is larger than the radius R of the convex part of the outer diameter side, at forming time of the permanent magnet, at first, the radius R of the convex part of the inner diameter side is formed so as to be smaller than the radius R of the outer diameter side. Thereafter, the permanent magnet is ground so that the radius R of the outer diameter side becomes smaller. This brings the same effect to the case of Fig. 1.

Please delete the paragraph at page 13, lines 6-10.

Please insert the following paragraph at page 14, between prenumbered lines 10-12:

The present invention is not limited to each of embodiments described above and shown in the drawings. The invention can be embodied by modifying the embodiments within the scope which does not deviate the intention, for example, the number of the permanent magnet 14 can be other than six.

REMARKS

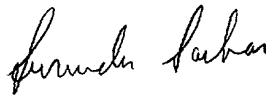
Favorable consideration of this application, as presently amended, is respectfully requested.

The present Preliminary Amendment is submitted to correct for informalities in the originally filed specification. The changes made to the specification are deemed to be self-evident from the original disclosure, and thus are not deemed to raise any issues of new matter.

The present application is believed to be in condition for a full and thorough examination on the merits. An early and favorable consideration of the present application is hereby respectfully requested.

Respectfully submitted,

OBLON, SPIVAK, McCLELLAND,
MAIER & NEUSTADT, P.C.



Gregory J. Maier
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Marked-Up Copy

Serial No:

Amendment Filed on:

07-24-01

IN THE SPECIFICATION

Please replace the paragraph at page 8, lines 14-20, as follows:

--Given a radius of an arc of the outer diameter side of the containing hole 13 provided to the rotor core 12 is R , and a radius of [an arc of the outer diameter side of the permanent magnet 14 is r , it is set as $R > r$] the outer circle of the rotor 10 is R' , it is set as $R < R'$. [An] The arc of the [outer convex part of the permanent magnet 14] outer diameter side of the containing hole 13 is set to be a part of a circumference of a circle whose center is the same to the center of the outer circle of the rotor 10. Consequently, the thickness t of the rotor core part 12a in the diameter direction has a constant value.--

Please replace the paragraph at page 9, lines 10-17, as follows:

--Although the magnetic orientation is set so that the focus should be located [on the outer diameter] outside of the rotor 10, the residual magnetic flux density cannot be decreased. This is because the compression direction at forming the permanent magnet becomes almost the same to the direction of the magnetic flux when the cross section of the permanent magnet 14 is shaped convex to the inner diameter side, and a radius R of the convex part of the inner diameter side is set to be smaller than a radius R of the outer diameter side as shown in Fig. 1.--

Please replace the paragraph at page 9, lines 18-25, as follows:

--On the contrary to the case of Fig. 1, when it is desired that the radius R of the convex part of the inner diameter side is larger than the radius R of the convex part of the

outer diameter side, at forming time of the permanent magnet, at first, the radius R of the convex part of the inner diameter side is formed so as to be smaller than the radius R of the outer diameter side. Thereafter, the permanent magnet is ground so that the radius R of the outer diameter side becomes [larger] smaller. This brings the same effect to the case of Fig. 1.--

Please delete the paragraph at page 13, lines 6-10.

--[The present invention is not limited to each of embodiments described above and shown in the drawings. The invention can be embodied by modifying the embodiments within the scope which does not deviate the intention, for example, the number of the permanent magnet 14 can be other than six.]--

Please insert the following paragraph at page 14, between prenumbered lines 10-12:

--The present invention is not limited to each of embodiments described above and shown in the drawings. The invention can be embodied by modifying the embodiments within the scope which does not deviate the intention, for example, the number of the permanent magnet 14 can be other than six.--

11/PR75

09/869322
JC18 Rec'd PCT/PTO 24 JUL 2001

English Translation for PCT/JP00/07926

SPECIFICATION

Permanent-magnet motor and Its Manufacturing Method

5

Technical Field

The present invention relates to a permanent-magnet motor and its manufacturing method used for such as an air conditioner and a compressor for a refrigerator.

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Background Art

Related Art 1.

Fig. 9 shows a conventional permanent-magnet motor.

15

In Fig. 9, a stator 1 consists of a circular stator core 2, plural teeth 3 provided to the stator core 2, and coils 4 wound around the teeth 3. The stator 1 is, for example, a distributed winding stator having stator winding of plural phases.

20

Inside of the stator 1, a rotor 10 is placed rotatably with a gap 5. The rotor 10 has a rotation axis 11 and a rotor core 12 provided around the rotation axis 11.

25

As shown in the figure, the permanent-magnet motor, in which a permanent magnet is used for a rotor of the motor, is formed by inserting plural permanent magnets 14, each of which has an arc in the view of its cross section, into a rotor core 12 having plural containing holes 13 provided near the peripheral part for inserting the plural permanent magnets. Each

permanent magnet 14 is placed so that the convex part should face to an outside.

Each permanent magnet 14 is magnetized so that magnetic orientation 15 of each piece should be parallel with a direct line connecting the center of the rotor 10 and the center part of the circumference of the permanent magnet 14, namely, the center of the magnetic orientation should be infinite. The rotor core 12 is made by multilayering multiple silicon steel plates respectively having the containing holes 13.

However, as for the permanent-magnet motor structured according to the first related art, the distribution of the magnetic flux density of the gap between the rotor 10 and the stator 1, generated by the permanent magnet 14, is in a wave form as shown in Fig. 11. Since this wave form is much different from sine wave, a problem is raised such as large cogging torque and much vibration and noise.

Related Art 2.

To solve the above problem, another technique has been developed as shown in Fig. 12. The rotor 10 of the figure is magnetized so that the focus of the magnetic orientation 15 of each piece of the permanent magnet 14 should be located outside of the rotor 10.

Using the above means, the magnetic flux density of the gap becomes high at the center part of the magnetic pole, while the density becomes low at both ends of the magnetic pole. Consequently, the distribution of the magnetic flux density of the gap resembles to the sine wave, which enables to decrease the cogging torque and also reduce the vibration and the noise.

However, in the motor structured as described above, the magnetic

orientation 15 should be focused to the convex part of the permanent magnet 14 on producing the permanent magnet 14. That is, the center of the magnetic orientation is placed in the opposite direction to the center of the arc formed due to the shape of the permanent magnet itself, which causes to
5 differentiate the direction of the magnetic flux from the direction of compression at manufacturing process of the permanent magnet. Consequently, the residual magnet flux density becomes low, accompanied by reducing the efficiency of the motor.

Related Art 3.

10 Another means to solve the problem raised in the above first related art can be considered as a structure shown in Fig. 14. In this rotor 10, the convex part of each piece of the permanent magnet 14 is placed so as to face the inside of the rotor core 12, and each piece of the permanent magnet is magnetized so that the focus of the magnetic orientation of each piece of the
15 permanent magnet 14 is located outside of the rotor 10.

Employing the above means, the distribution of the magnetic flux density of the gap is high at the center part of the magnetic pole and low at the both ends. That is, the distribution becomes close to the sine wave as shown in Fig. 15. Accordingly, the cogging torque can be decreased, the
20 vibration and the noise can be reduced. On manufacturing the permanent magnet 14, the magnetic orientation 15 can be focused at the concave part of the permanent magnet 14. Namely, the center of the magnetic orientation becomes in the same direction to the center of the arc formed due to the shape of the permanent magnet itself, and therefore, the direction of
25 compression at producing the permanent magnet also becomes the same to

the direction of the magnetic flux. The residual magnetic flux density is not lowered nor the efficiency of the motor becomes worse.

However, in the structure of the rotor according to the third related art explained above, the thickness of a rotor core part 12a which separates the gap 5 and each of the permanent magnet 14 becomes increased, and the magnetic resistance becomes low. Consequently, among magnetic flux 20 generated by electric current of the coil 4, the amount of the magnetic flux which passes through the rotor core part 12a and short-circuits with the teeth 3 of the stator core 2 becomes large. Accordingly, the torque ripple generated by the fundamental wave component and higher harmonic wave component also becomes increased, which causes to enlarge the vibration and the noise.

The present invention aims to provide, for example, a permanent-magnet motor, having a permanent magnet, which can reduce the vibration and the noise without decreasing the efficiency of the motor and a manufacturing method for the permanent-magnet motor.

Disclosure of the Invention

According to the preferred embodiment of the present invention, a permanent-magnet motor and a manufacturing method for the permanent-magnet having:

a stator having stator winding of plural phases; and

a rotor facing to inside of the stator across a gap part, and having a rotor core and a permanent magnet provided to the rotor core,

wherein the permanent magnet is made so as to have both of a

convex part to an inner diameter side and a convex part to an outer diameter side in a cross section taken vertically to an axis; and

wherein a focus of magnetic orientation of each magnetic pole of the permanent magnet is located outside of the rotor.

Further, the rotor is formed by a rotor core assembly made by multilayering multiple pieces of core laminations, each having plural containing holes for inserting the permanent magnets and the permanent magnets are inserted into the containing holes for inserting the permanent magnets and a thickness of the rotor core, which separates the permanent magnet and the gap, is made within $\pm 30\%$ of a thickness of the rotor core lamination.

Further, the rotor is formed by including the permanent magnets in an outer peripheral part of the rotor core and a non-magnetic protect pipe is attached around the permanent magnets.

Further, when a radius of an arc of an outer diameter side of the containing hole provided to the rotor core for inserting the permanent magnet is R , and a radius of an arc of an outer diameter side of the permanent magnet inserted into the containing hole is r , it is set as $R < r$.

Further, in the permanent-magnet motor, in which a thickness of the rotor core separating the permanent magnet and the gap part is made within $\pm 30\%$ of a thickness of the multiple rotor core laminations, the stator is a concentrated winding stator made by directly winding a coil around a teeth part of the stator.

Further, a radius of the convex part to the inner diameter side of the permanent magnet is smaller than a radius of the convex part to the outer

diameter side of the permanent magnet.

Yet further, a straight line part is provided to each of a part of an arc of an inner diameter side of the containing hole for inserting the permanent magnet and a part of an arc of an inner diameter side of the permanent
5 magnet.

Brief Explanation of the Drawings

Fig. 1 shows the first embodiment and illustrates a permanent-magnet motor.

10 Fig. 2 shows the first embodiment and illustrates a magnetic orientation status of the permanent magnet.

Fig. 3 shows the first embodiment and is a distribution diagram of magnetic flux density.

Fig. 4 shows the first embodiment and is a partial enlarged view of
15 Fig. 1.

Fig. 5 shows the second embodiment and illustrates a rotor of the permanent-magnet motor.

Fig. 6 shows the third embodiment and illustrates the rotor of a single pole.

20 Fig. 7 shows the fourth embodiment and illustrates the permanent-magnet motor.

Fig. 8 shows the fifth embodiment and illustrates the rotor of a single pole.

Fig. 9 shows a conventional permanent-magnet motor.

25 Fig. 10 shows magnetic orientation status of the conventional

permanent-magnet motor.

Fig. 11 is a distribution diagram of magnetic flux density.

Fig. 12 shows another magnetic orientation status of the conventional permanent-magnet motor.

5 Fig. 13 is a distribution diagram of magnetic flux density..

Fig. 14 shows another magnetic orientation status of the conventional permanent-magnet motor.

Fig. 15 is a distribution diagram of magnetic flux density..

Fig. 16 is a partial enlarged view of Fig. 14.

10 Best Mode for Carrying out the Invention

Embodiment 1.

In the following, the first embodiment of the present invention will be explained by referring to the figures.

15 Figs. 1 through 4 shows the first embodiment: Fig. 1 shows a permanent-magnet motor; Fig. 2 shows magnetic orientation status of a permanent magnet; Fig. 3 is a distribution diagram of magnetic flux density; and Fig. 4 shows a partial enlarged view of Fig. 1.

20 In Fig. 1, a stator 1 includes a circular stator core 2, plural teeth 3 provided to the stator core 2, and coils 4 wound around these teeth 3. The stator 1 is, for example, a distributed winding stator having stator winding of plural phases.

25 Inside of the stator 1, a rotor 10 is placed rotatably with a gap 5. The rotor 10 has a rotation axis 11 and a rotor core 12 provided around the rotation axis 11. A permanent magnet is inserted from the direction of the

axis into a containing hole 13 for inserting the permanent magnet. The rotor core 12 has a multilayered rotor core assembly formed by multilayering multiple pieces of silicon steel plates, each of which is called a punched rotor core lamination and has the containing holes 13 punched, in the direction of
 5 the rotation axis 11 (that is, vertically to a sheet of Fig. 1).

The containing hole 13 provided to the rotor core 12 has a shape being convex to both inner diameter side and outer diameter side in the cross section taken vertically to the rotation axis 11. Further, the thickness t in the diameter direction of a rotor core part 12a, which separates the
 10 permanent magnet 14 and the gap 5, is set within $\pm 30\%$ of the thickness of the rotor core lamination. For example, if the thickness of one piece of the rotor core lamination is 0.5mm, the thickness t of the rotor core part 12a in the diameter direction becomes 0.35mm through 0.65mm.

Given a radius of an arc of the outer diameter side of the containing
 15 hole 13 provided to the rotor core 12 is R , and a radius of an arc of the outer diameter side of the permanent magnet 14 is r , it is set as $R > r$. An arc of the outer convex part of the permanent magnet 14 is set to be a part of a circumference of a circle whose center is the same to the center of the outer circle of the rotor 10. Consequently, the thickness t of the rotor core part
 20 12a in the diameter direction has a constant value.

Further, the permanent magnet 14 has a substantially similar shape to the containing hole 13 and is magnetized so that the N pole and the S pole are located alternately and so that the focus of magnetic orientation of each part is located outside of the rotor 10 as shown in Fig. 2.

25 In the permanent-magnet motor structured as described above, the

distribution of the magnetic flux density of the gap caused by the permanent magnet 14 becomes large at the center part of the magnetic pole and small at the both ends, which becomes resemble to the sine wave as shown in Fig. 3. Accordingly, the cogging torque can be decreased, and the vibration and the noise can be reduced.

In case of Fig. 2, the focus of the magnetic orientation 15 is one place, however, the same effect can be obtained even if the focus becomes placed separately at multiple places as long as the focus is placed outside of the rotor 10.

Although the magnetic orientation is set so that the focus should be located on the outer diameter of the rotor 10, the residual magnetic flux density cannot be decreased. This is because the compression direction at forming the permanent magnet becomes almost the same to the direction of the magnetic flux when the cross section of the permanent magnet 14 is shaped convex to the inner diameter side, and a radius R of the convex part of the inner diameter side is set to be smaller than a radius R of the outer diameter side as shown in Fig. 1.

On the contrary to the case of Fig. 1, when it is desired that the radius R of the convex part of the inner diameter side is larger than the radius R of the convex part of the outer diameter side, at forming time of the permanent magnet, at first, the radius R of the convex part of the inner diameter side is formed so as to be smaller than the radius R of the outer diameter side. Thereafter, the permanent magnet is ground so that the radius R of the outer diameter side becomes larger. This brings the same effect to the case of Fig. 1.

As has been described, since the residual magnetic flux density of the permanent magnet 14 itself is not decreased, the efficiency of the motor is not lowered, either.

Further, both the containing hole 13 and the permanent magnet 14 have a convex shape to the outer diameter side, and the thickness t in the diameter direction of the rotor core part 12a, which separates the gap 5 and each piece of the permanent magnet 14, is made thin. Therefore, the magnetic resistance of the rotor core part 12a becomes large, and the number of magnetic flux passing through the rotor core part 12a, which separates the gap 5 and each piece of the permanent magnet 14, can be limited as shown in Fig. 4. Consequently, among the magnetic flux 20 generated by electric current of the coil 4, an amount of the magnetic flux short-circuited between the rotor core part 12a and the teeth 3 of the stator core 2 can be decreased. The torque ripple generated by the higher harmonic wave component of the magnetic flux can be decreased, which enables to reduce the vibration and the noise.

In the above case, the thickness t in the diameter direction of the rotor core part 12a is desired to be within $\pm 30\%$ of the thickness of the lamination in consideration of the characteristic of the rotor core lamination and the magnetic resistance. Namely, making the thickness t of the rotor core part 12a in the diameter direction too small causes to destroy the rotor core part 12a on punching the rotor core lamination. On the contrary, if the thickness t of the rotor core part 12a in the diameter direction is made too large, the number of the magnetic flux passing through the rotor core part 12a separating the gap 5 and each piece of the permanent magnet 14 cannot

be decreased.

Embodiment 2.

Hereinafter, the second embodiment of the present invention will be explained referring to the figure.

5 Fig. 5 shows the second embodiment and illustrates the rotor of the permanent-magnet motor. As shown in Fig. 5, the permanent magnet 14 is placed at the outer peripheral part of the rotor core 12, and the permanent magnet 14 is protected by attaching a non-magnetic pipe 16 around the permanent magnet. By this structure, the magnetic flux short-circuited
10 between the rotor core 12 and the stator core 2 can be further decreased, and accordingly, the torque ripple can be also decreased, which enables to reduce the vibration and the noise.

Embodiment 3.

Hereinafter, the third embodiment of the present invention will be
15 explained referring to the figure.

Fig. 6 shows the third embodiment and illustrates one pole of the rotor. As shown in the figure, when the radius of the arc of the outer diameter side of the containing hole 13 provided to the rotor core 12 is R , and the radius of the arc of the outer diameter side of the permanent magnet 14 is r , it is set as $R < r$. Therefore, the rotor core part 12a separating the permanent magnet 14 and the gap 5 is not contacted to the permanent magnet 14 at around the center part of the circumference of the permanent magnet 14. Large moment of inertia influenced to both ends from around the center part of the rotor core part 12a due to the centrifugal force
20 generated by high-speed rotation of the rotor 10 can be taken out, which
25

enables to decrease shearing stress. Consequently, the present embodiment can prevent deformation and break of the rotor.

Embodiment 4.

Hereinafter, the fourth embodiment of the present invention will be explained referring to the figure.

Fig. 7 shows the fourth embodiment and illustrates the permanent-magnet motor. In the first through third embodiments, the stator is the distributed winding stator. As shown in Fig. 7, the stator 1 of the present embodiment is a concentrated winding stator including a circular stator core 2, plural teeth 3 formed on the stator core 2, and a coil 4 directly wound around the teeth 3, which brings the following advantage.

In the concentrated winding stator, among the magnetic flux generated by the electric current of the coil 4, the magnetic flux, which passes through the rotor core part 12a separating the gap 5 and each piece of the permanent magnet 14 and short-circuits between the rotor core part 12a and the teeth 3 of the stator core 2, influences to the vibration and the noise more than the distributed winding. Therefore, more efficient reduction of the torque ripple, namely, of the vibration and the noise can be obtained by setting the thickness t in the diameter direction of the rotor core part 12a, which separates the gap 5 and each piece of the permanent magnet 14, to be within $\pm 30\%$ of the thickness of the rotor core lamination.

Recently, another type of the concentrated winding stator has been proposed for obtaining higher efficiency due to the high coil space factor of the coil 4: such as single winding of the teeth 3 made by dividing the stator core 2; and directly winding the teeth by opening and holding the iron core to

straight or inversely warped. These kinds of stator have a problem that the rigidity of the stator has been weakened due to the division, which may cause to enlarge the vibration and the noise. Accordingly, it is more efficient to employ the present embodiment to increase the efficiency and reduce the vibration and the noise.

The present invention is not limited to each of embodiments described above and shown in the drawings. The invention can be embodied by modifying the embodiments within the scope which does not deviate the intention, for example, the number of the permanent magnet 14 can be other than six.

Embodiment 5.

In the following, the fifth embodiment of the present invention will be explained referring to the figure.

Fig. 8 shows the fifth embodiment and illustrates one pole of the rotor. As shown in the figure, a straight line part 30 is provided to each of a part of the arc of inner diameter side of the containing hole 13 of the permanent magnet provided to the rotor core 12 and a part of the arc of the inner diameter side of the permanent magnet 14, which brings the following advantages.

Since the straight line part 30 is provided to the part of the arc of the permanent magnet 14, a difference of the thickness between the center part of the permanent magnet and the both ends is decreased. Accordingly, a difference of the compression ratio at producing the permanent magnet is lowered, which reduces defective product having a clack or a chip.

Further, by providing the straight line part 30 to the part of the arc of

the permanent magnet 14, the permanent magnet can fit to the equipment at grinding process after forming, which enables to easily obtain the accuracy. Accordingly, the number of cases producing the permanent magnet 14 having wrong size can be reduced, and further, the number of cases of defective
5 insertion into the rotor core 12 at inserting process can be also reduced.

Yet further, since the straight line part 30 is provided to the arc of the inner diameter side, not to the outer diameter side, the amount of the magnetic flux short-circuited between the rotor core part 12a and the teeth 3 of the stator core 2 does not change, nor the torque ripple generated by the
10 higher harmonic wave component of the magnetic flux increases.

Industrial Applicability

According to the preferred embodiment of the present invention, in the permanent-magnet motor, the permanent magnet is made so as to have a
15 shape in which both of the inner diameter side and the outer diameter side are convex in the cross section taken vertically to the axis, and further, the focus of the magnetic orientation of each magnetic pole of the permanent magnet is located outside of the rotor. Therefore, the distribution of the magnetic flux density of the gap is high at the center part and low at both
20 ends, which resembles the sine wave. Accordingly, the cogging torque can be decreased, and the vibration and the noise can be reduced. Further, since the magnet can be produced without decreasing the residual magnetic flux density, the efficiency of the motor cannot be lowered.

Further, in the rotor, the rotor core assembly is formed by
25 multilayering multiple pieces of rotor core laminations, each having plural

containing holes for inserting the permanent magnets. The permanent magnet is inserted into the containing hole for inserting the permanent magnet, and further, the thickness of the rotor core, which separates the permanent magnet and the gap, is made within $\pm 30\%$ of the thickness of the rotor core lamination. Therefore, within the magnetic flux generated by the electric current of the coil of the stator, the amount of the magnetic flux short-circuited between the rotor core part and the teeth of the stator core can be decreased. Consequently, the torque ripple generated by the higher harmonic wave component of the magnetic flux can be decreased, and the vibration and the noise can be reduced.

Further, since the rotor is formed by inserting the permanent magnet to the outer peripheral part of the rotor core and attaching the non-magnetic protect pipe around the permanent magnet, the amount of the magnetic flux short-circuited between the rotor core part and the teeth of the stator core can be further decreased.

Further, when the radius of the arc of the outer diameter side of the containing hole for inserting the permanent magnet provided to the rotor core is R , and the radius of the arc of the outer diameter side of the permanent magnet inserted into the containing hole is r , it is set as $R < r$. Consequently, the rotor core part separating the permanent magnet and the gap does not contact to the permanent magnet at around center part in the circumference of the permanent magnet, which prevents the deformation and the break of the rotor due to the centrifugal force generated by high-speed rotation of the rotor.

Further, in the permanent-magnet motor, the thickness of the rotor

core separating the permanent magnet and the gap is set within $\pm 30\%$ of the thickness of the rotor core lamination, and the concentrated winding stator made by directly winding the coil is provided to the teeth part of the stator. Therefore, the reduction of the torque ripple, namely, of the vibration and the noise can be made more efficiently by setting the thickness of the rotor core part separating the gap and the permanent magnet in the diameter direction within $\pm 30\%$ of the thickness of the rotor core lamination.

Further, since the radius of the convex of the inner diameter side of the permanent magnet is made smaller than the radius of the convex of the outer diameter side, the compression direction at forming the permanent magnet becomes almost the same to the direction of the magnetic flux, and the residual magnetic flux density is not decreased.

Further, the straight line parts are provided to the part of the containing hole for inserting the permanent magnet and the part of the arc of the inner diameter side of the permanent magnet, a difference of the compression ratio at producing the permanent magnet is decreased, which can reduce defective product having a clack or a chip.

Further, the permanent magnet can fit to the equipment at grinding process after forming, which enables to easily obtain the accuracy. Accordingly, the number of cases producing the permanent magnet having wrong size can be decreased, and further, the number of defective insertion into the rotor core at inserting process can be also decreased.

Yet further, since the amount of the magnetic flux short-circuited between the rotor core and the teeth of the stator core is not increased, nor

the torque ripple generated by the higher harmonic wave component of the magnetic flux increases.

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Claims

1. A permanent-magnet motor comprising:

a stator having stator winding of plural phases; and

a rotor facing to inside of the stator across a gap part, and having a
5 rotor core and a permanent magnet provided to the rotor core,

wherein the permanent magnet is made so as to have both of a
convex part to an inner diameter side and a convex part to an outer diameter
side in a cross section taken vertically to an axis; and

wherein a focus of magnetic orientation of each magnetic pole of the
10 permanent magnet is located outside of the rotor.

2. The permanent-magnet motor of claim 1, wherein the rotor is formed
by a rotor core assembly made by multilayering multiple pieces of core
laminations, each having plural containing holes for inserting the
permanent magnets and the permanent magnets are inserted into the
15 containing holes for inserting the permanent magnets; and

wherein a thickness of the rotor core, which separates the permanent
magnet and the gap, is made within $\pm 30\%$ of a thickness of the rotor core
lamination.

3. The permanent-magnet motor of claim 1, wherein the rotor is formed
20 by including the permanent magnets in an outer peripheral part of the rotor
core and a non-magnetic protect pipe is attached around the permanent
magnets.

4. The permanent-magnet motor of claim 1, wherein a containing hole
is provided to the rotor core for inserting the permanent magnet; and

25 wherein when a radius of an arc of an outer diameter side of the

containing hole is R , and a radius of an arc of an outer diameter side of the permanent magnet inserted into the containing hole is r , it is set as $R < r$.

5. The permanent-magnet motor of claim 1, wherein the stator is a concentrated winding stator made by directly winding a coil around a teeth
5 part of the stator.

6. The permanent-magnet motor of claim 1, wherein a radius of the convex part to the inner diameter side of the permanent magnet is smaller than a radius of the convex part to the outer diameter side of the permanent magnet.

10 7. The permanent-magnet motor of claim 1, wherein a straight line part is provided to each of a part of an arc of an inner diameter side of the containing hole for inserting the permanent magnet and a part of an arc of an inner diameter side of the permanent magnet.

8. A permanent-magnet motor comprising:

15 a stator having stator winding of plural phases; and

a rotor facing to inside of the stator across a gap part, and having a rotor core and a permanent magnet provided to the rotor core, and

wherein the permanent magnet is made so as to have both of a convex part to an inner diameter side and a convex part to an outer diameter
20 side in a cross section taken vertically to an axis.

9. A method for manufacturing a permanent-magnet motor including a stator having stator winding of plural phases and a rotor facing to inside of the stator across a gap part, and having a rotor core and a permanent magnet provided to the rotor core, the method comprising:

25 making the permanent magnet so as to have both a convex part to an

inner diameter side and a convex part to an outer diameter side in a cross section taken vertically to an axis.

10. The method for manufacturing the permanent-magnet motor of claim 9, the method comprising:

5 forming a rotor core assembly by multilayering multiple rotor core laminations, each having plural containing holes for inserting the permanent magnets;

inserting the permanent magnets into the plural containing holes for inserting the permanent magnets; and

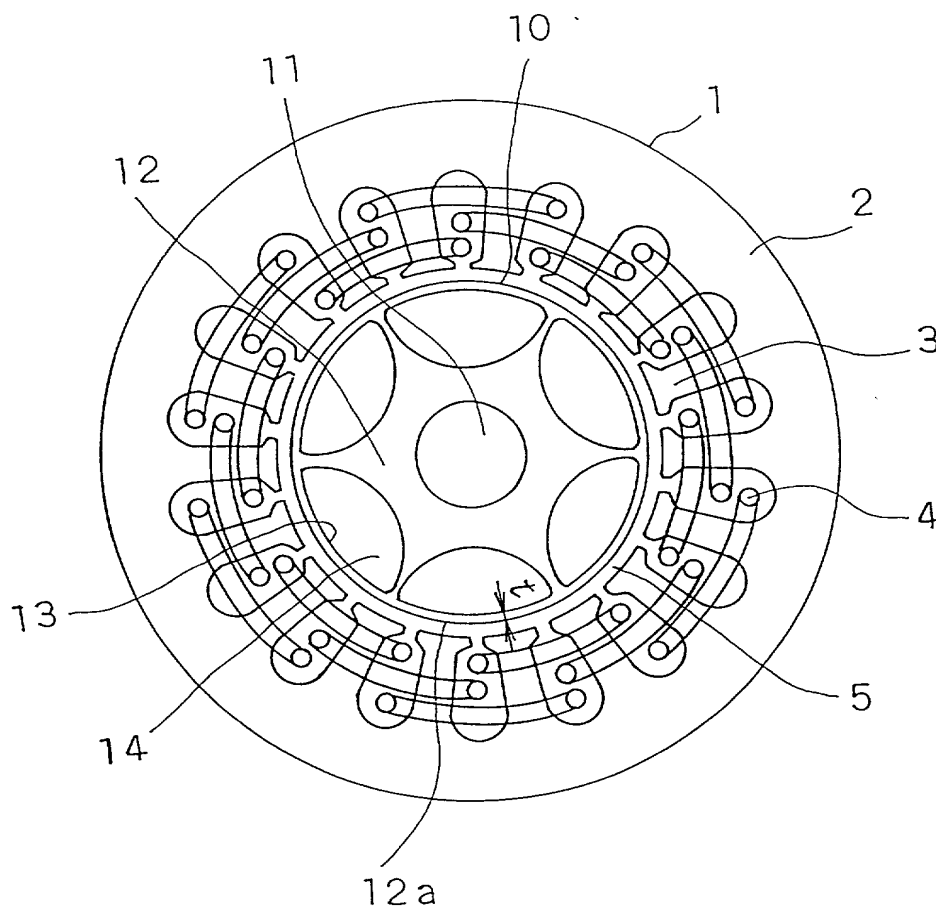
10 wherein a thickness of the rotor core, which separates the permanent magnet and the gap part, is made within $\pm 30\%$ of a thickness of the multiple rotor core laminations.

Abstract

To provide a permanent-magnet motor having a permanent magnet which can reduce the vibration and the noise without lowering the efficiency of the motor, the permanent-magnet motor according to the present invention has a stator 1 having stator winding of plural phases, a rotor 10 having a stator core 12 facing to inside of the stator across a gap part and a permanent magnet 14 provided to the rotor core. In the permanent-magnet motor, the permanent magnet 14 is made to have both a convex part to the inner diameter side and a convex part to the outer diameter side in the cross section taken vertically to the rotation axis, and a focus of magnetic orientation of each magnetic pole of the permanent magnet is located outside of the rotor 10.

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Fig.1



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Fig.2

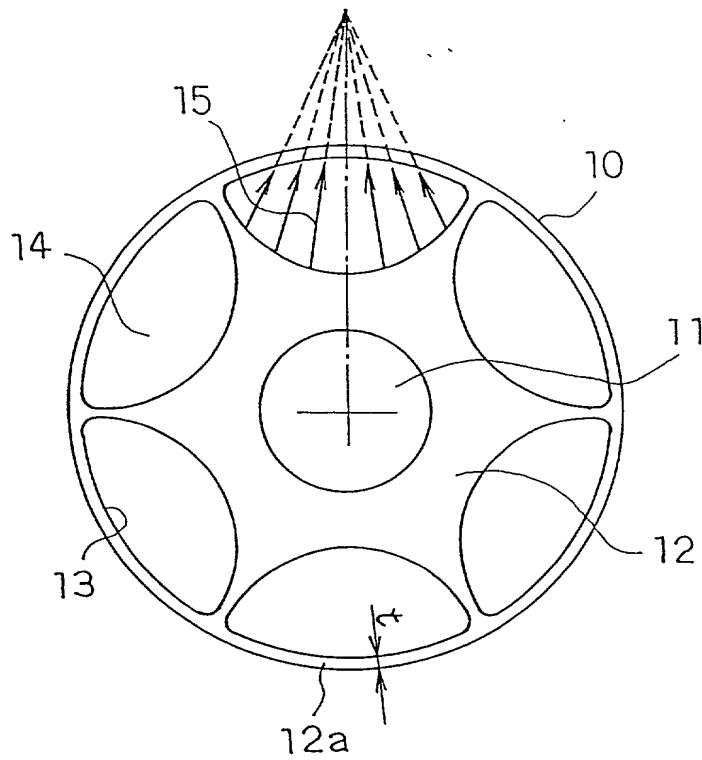
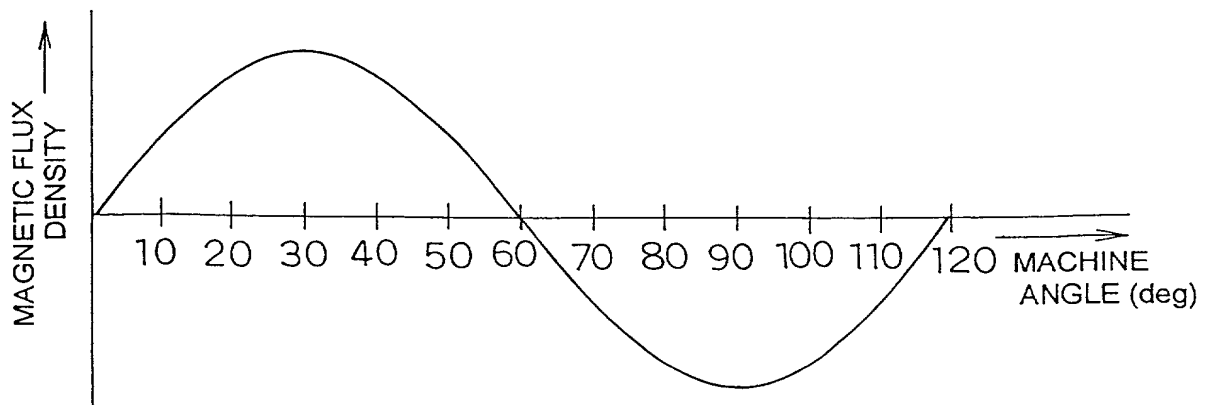
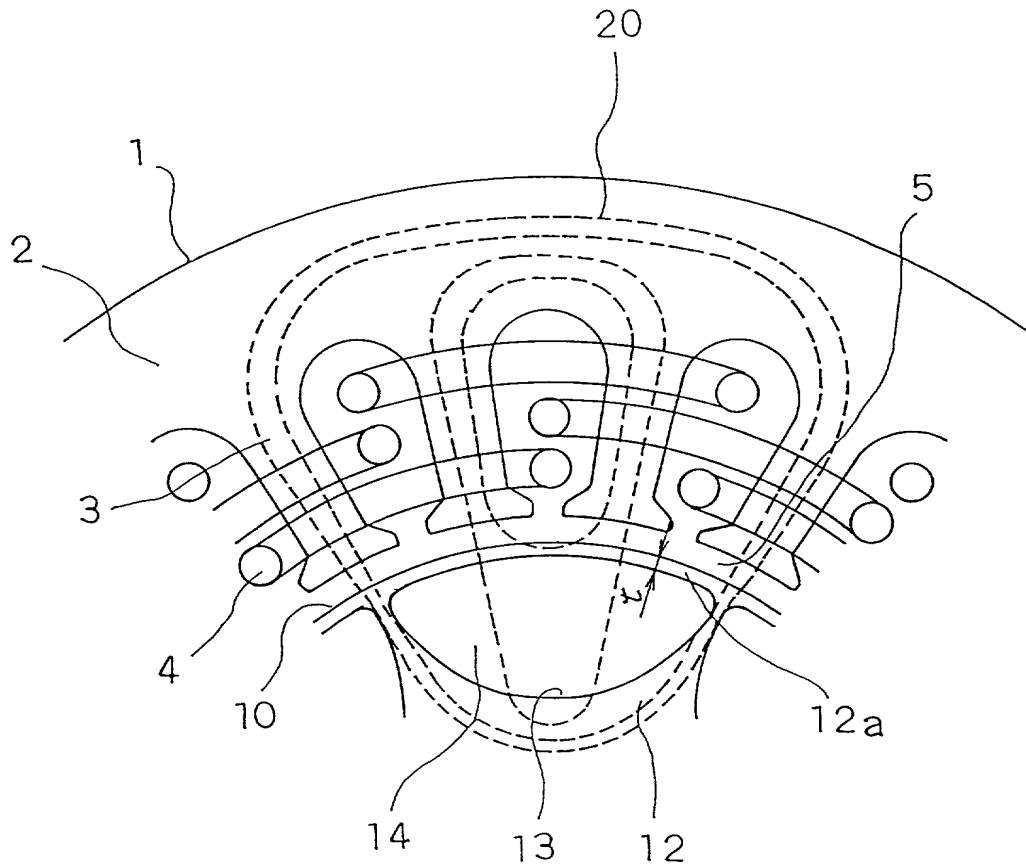


Fig.3



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Fig.4



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Fig.5

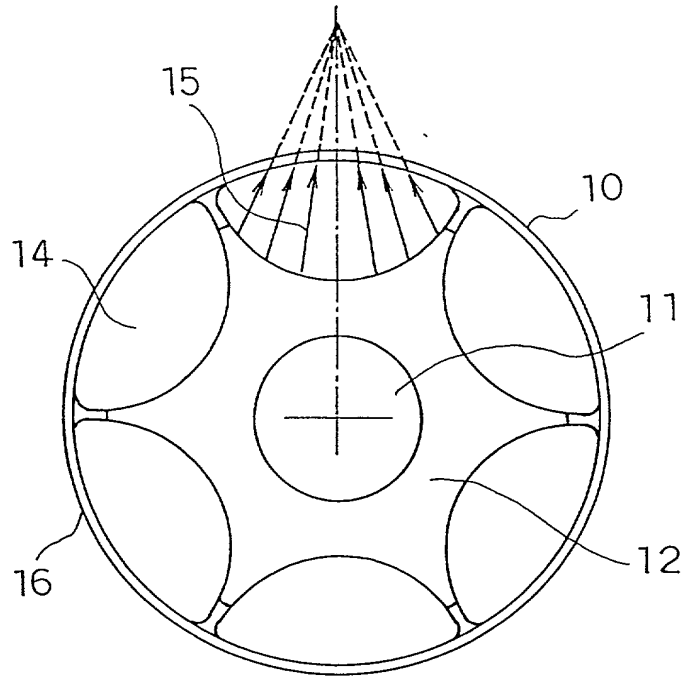
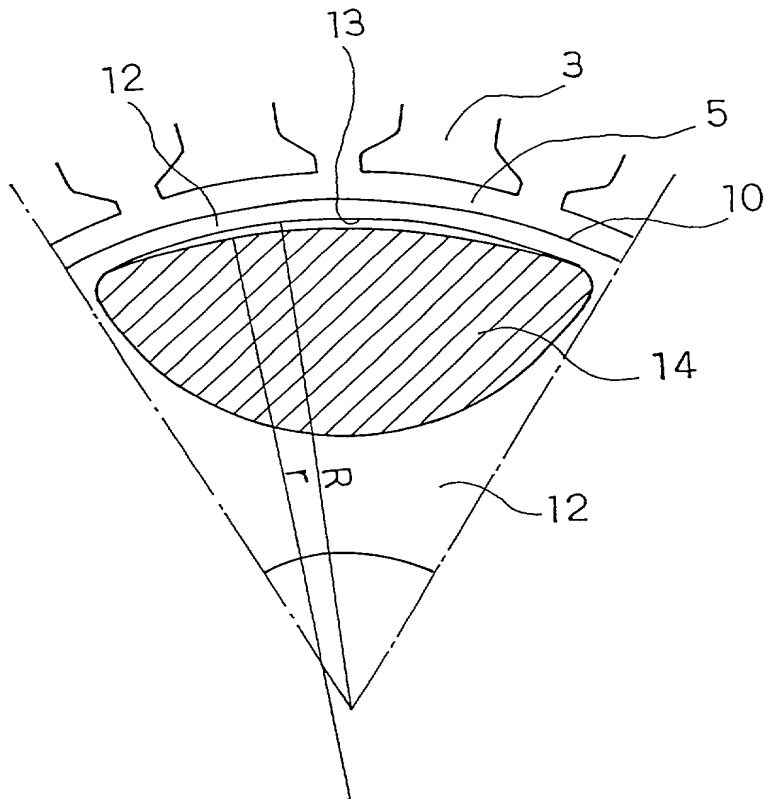
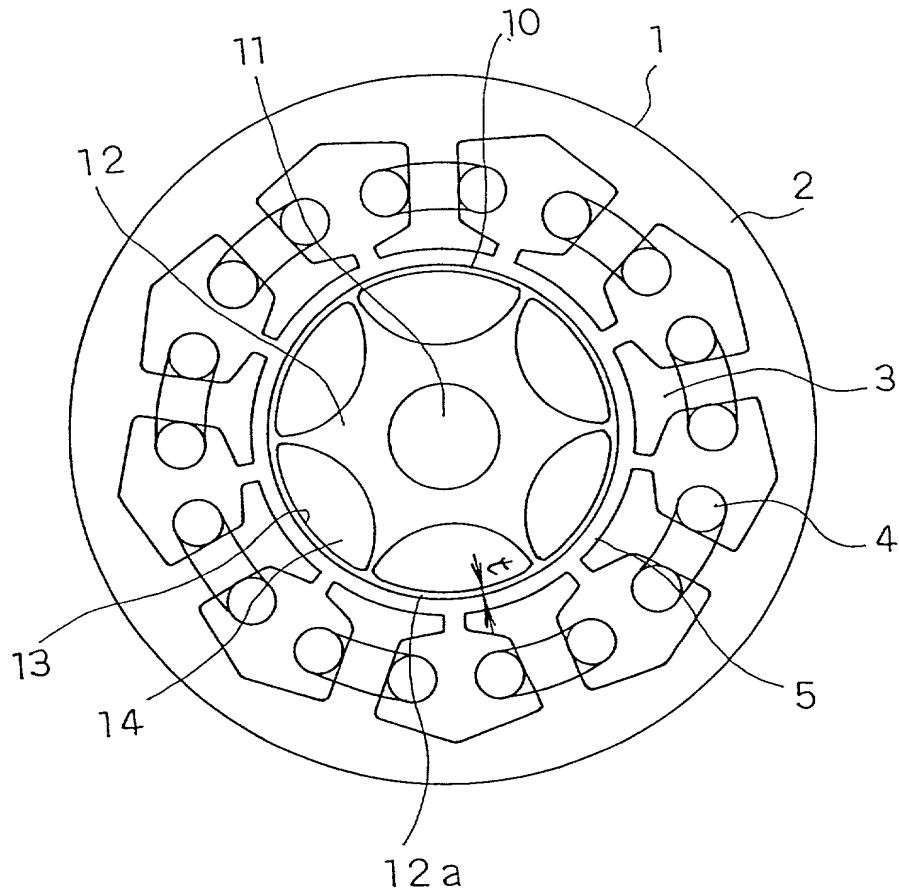


Fig.6



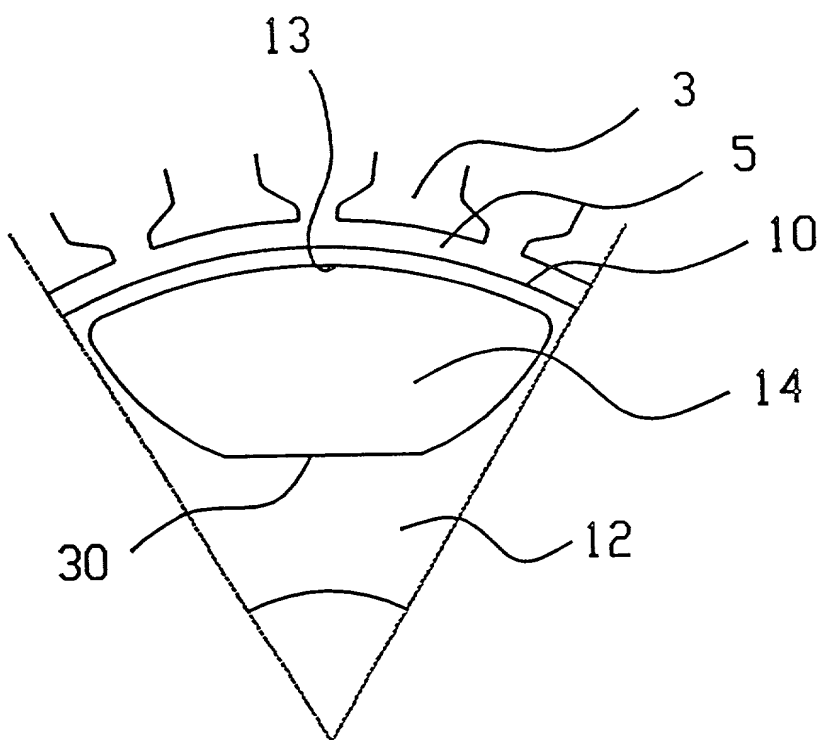
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Fig.7



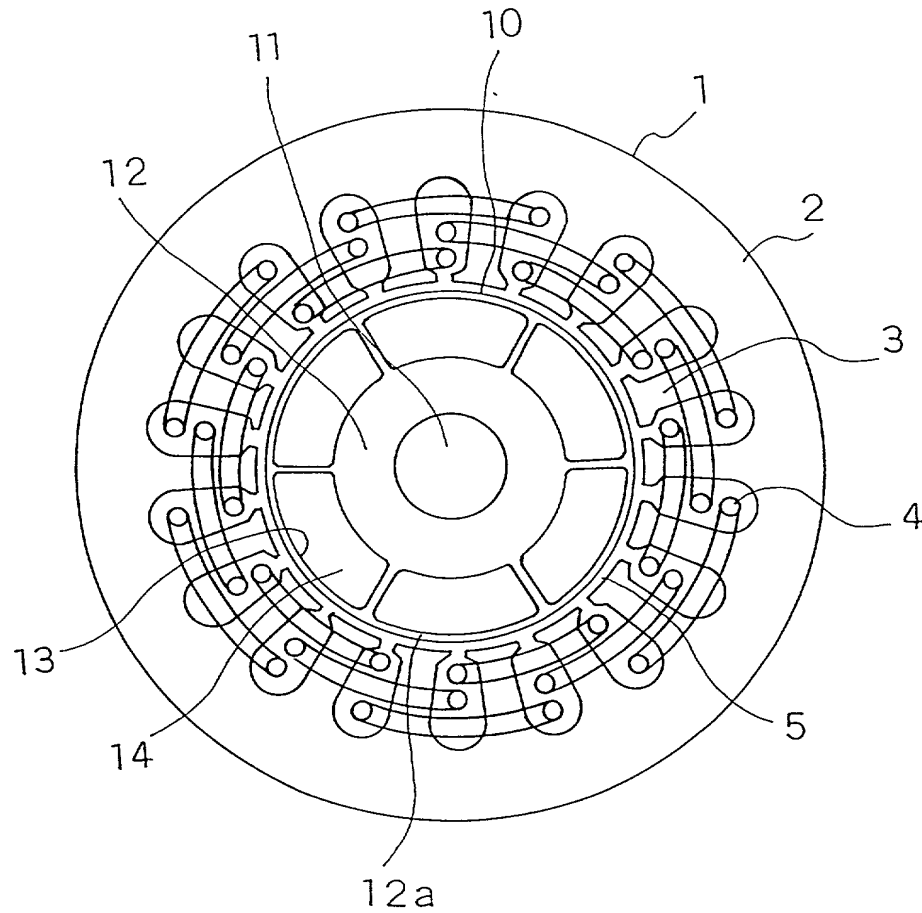
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Fig.8



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Fig.9



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Fig.10

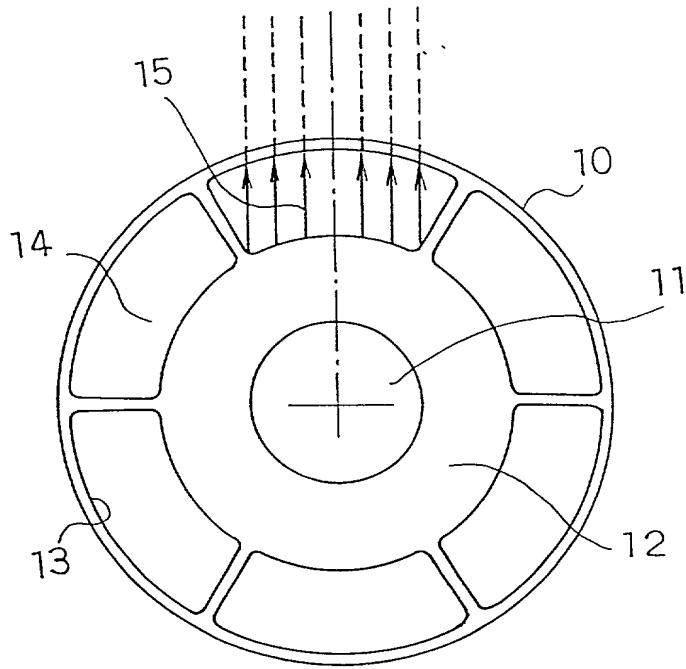
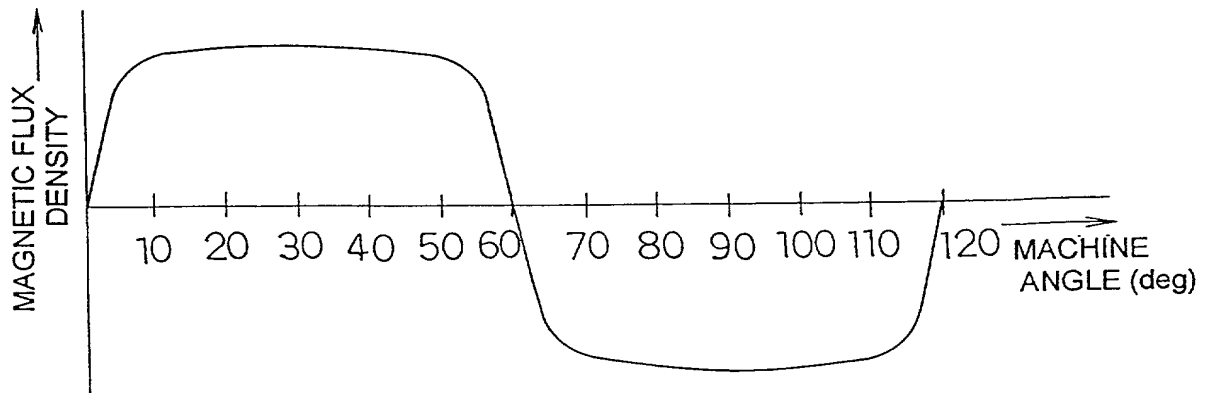


Fig.11



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Fig.12

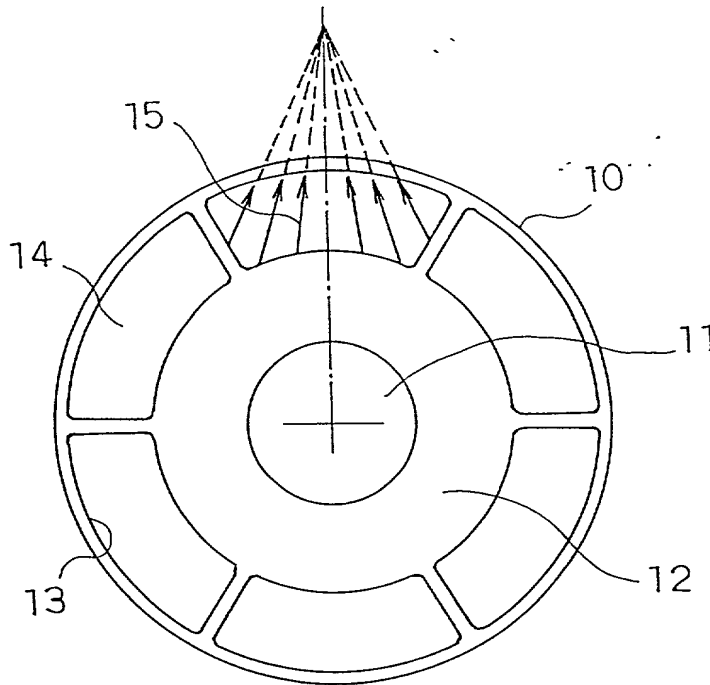
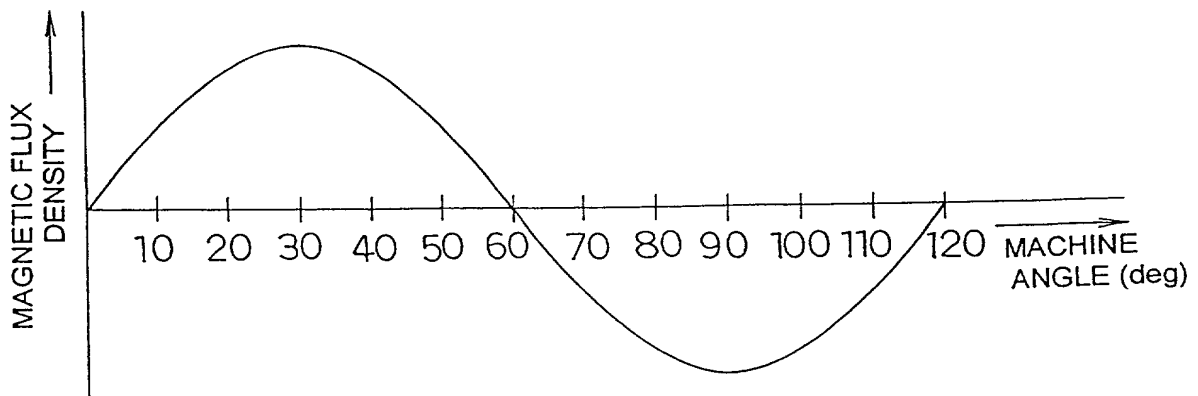


Fig.13



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Fig.14

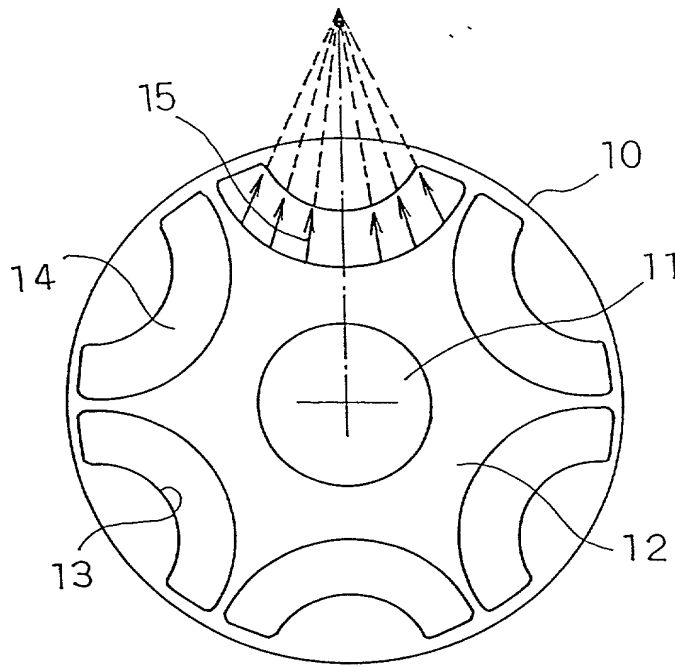
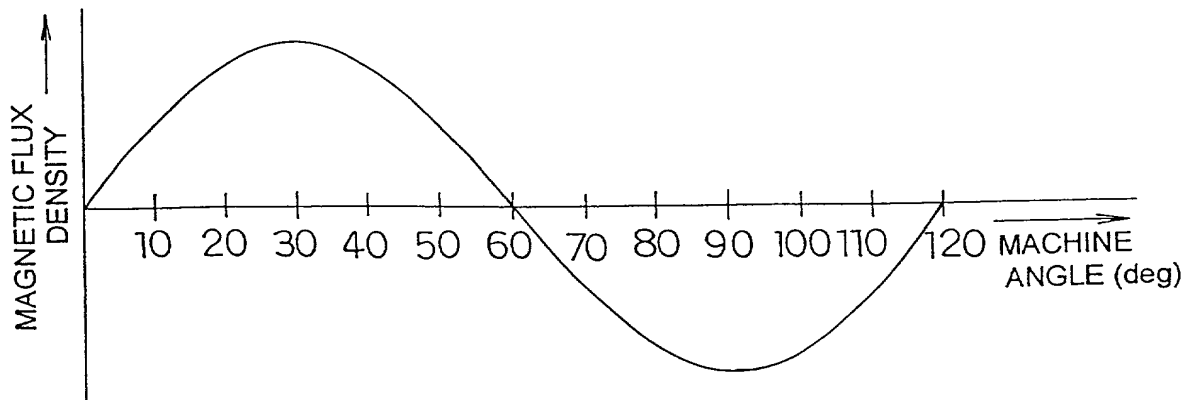
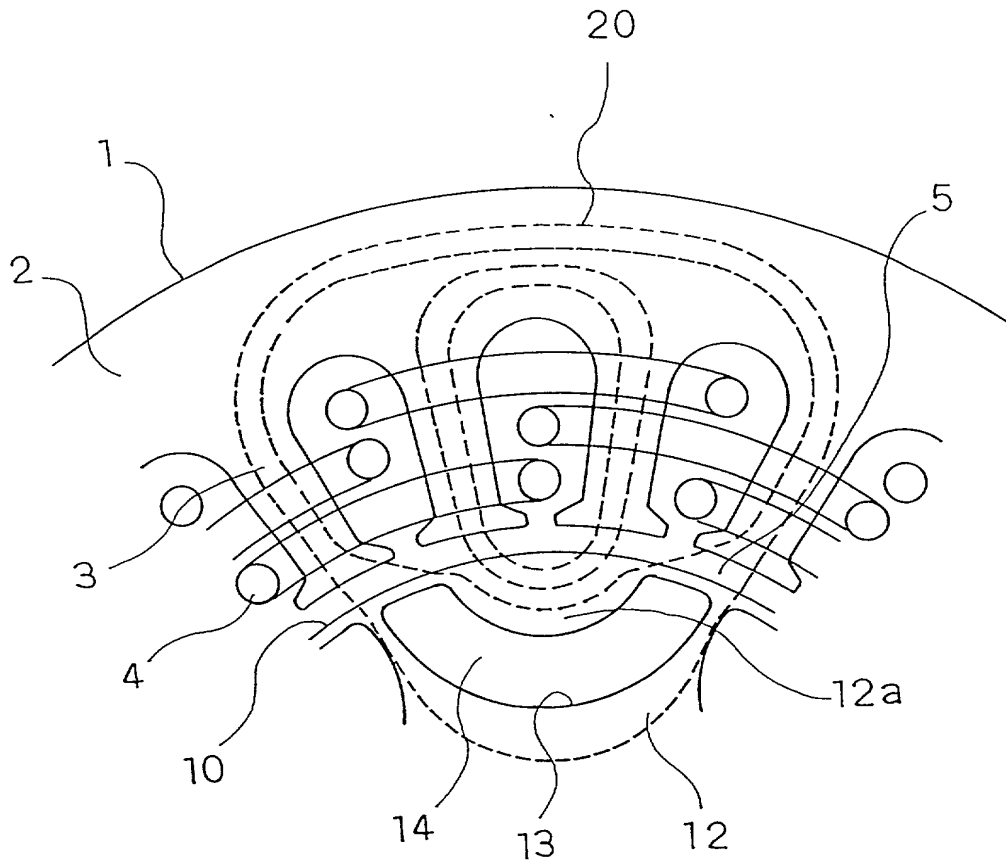


Fig.15



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Fig.16



Declaration and Power of Attorney For Patent Application

特許出願宣告書及び委任状

Japanese Language Declaration

日本語宣告書

下記の氏名の発明者として、私は以下の通り宣言します。

私の住所、私書箱、国籍は下記の私の氏名の後に記載された通りです。

下記の名称の発明に関して請求範囲に記載され、特許出願している発明内容について、私が最初かつ唯一の発明者（下記の氏名が一つの場合）もしくは最初かつ共同発明者（下記の名称が複数の場合）であると信じています。

上記発明の明細書は、

☐ 本書に添付されています。

☐ __月__日に提出され、米国出願番号または特許協定条約国際出願番号を____とし、
(該当する場合) _____に訂正されました。

私は、特許請求範囲を含む上記訂正後の明細書を検討し、内容を理解していることをここに表明します。

私は、連邦規則法典第37編第1条56項に定義されるとおり、特許資格の有無について重要な情報を開示する義務があることを認めます。

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

Permanent-Magnet Motor and
its Manufacturing Method

the specification of which

☐ is attached hereto.

☒ was filed on 10/November/2000
as United States Application Number or
PCT International Application Number
PCT/JP00/07926 and was amended on
_____ (if applicable).

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56.

Japanese Language Declaration

(日本語宣告書)

私は、米国法典第 35 編 119 条(a)-(d)項又は 365 条(b)項に基づき下記の、米国以外の国の少なくとも一ヶ国を指定している特許協力条約 365(a)項に基づく国際出願、又は外国での特許出願もしくは発明者証の出願についての外国優先権をここに主張するとともに、優先権を主張している、本出願の前に出願された特許または発明者証の外国出願を以下に、枠内をマークすることで、示しています。

Prior Foreign Application(s)

外国での先行出願

<u>Hei 11-353721</u> ✓	<u>Japan</u> ✓
(Number) (番号)	(Country) (国名)
_____	_____
(Number) (番号)	(Country) (国名)

私は、第 35 編米国法典 119 条(e)項に基づいて下記の米国特許出願規定に記載された権利をここに主張いたします。

<u>_____</u>	<u>_____</u>
(Application No.) (出願番号)	(Filing Date) (出願日)

私は、下記の米国法典第 35 編 120 条に基づいて下記の米国特許出願に記載された権利、又は米国を指定している特許協力条約 365 条(e)に基づく権利をここに主張します。また、本出願の各請求範囲の内容が米国法典第 35 編 112 条第 1 項又は特許協力条約で規定された方法で先行する米国特許出願に開示されていない限り、その先行米国出願書提出日以降で本出願書の日本国内または特許協力条約国際提出日までの期間中に入手された、連邦規則法典第 37 編 1 条 56 項で定義された特許資格の有無に関する重要な情報について開示義務があることを認識しています。

<u>_____</u>	<u>_____</u>
(Application No.) (出願番号)	(Filing Date) (出願日)

<u>_____</u>	<u>_____</u>
(Application No.) (出願番号)	(Filing Date) (出願日)

私は、私自身の知識に基づいて本宣告書で私が行なう表明が真実であり、かつ私の入手した情報と私の信じることに基づく表明が全て真実であると信じていること、さらに故意になされた虚偽の表明及びそれと同等の行為は米国法典第 18 編第 1001 条に基づき、罰金または拘禁、もしくはその両方により処罰されること、そしてそのような故意による虚偽の声明を行えば、出願した、又は既に許可された特許の有効性が失われることを認識し、よってここに上記のごとく宣誓を致します。

I hereby claim foreign priority under Title 35, United States Code, Section 119 (a)-(d) or 365(b) of any foreign application(s) for patent or Inventor's certificate, or Section 365(a) of any PCT international application which designated at least one country other than the United States, listed below and have also identified below, by checking the box, any foreign application for patent or Inventor's certificate, or PCT International application having a filing date before that of the application on which priority is claimed.

Priority Claimed
優先権主張

<u>13/December/1999</u> ✓	<input checked="" type="checkbox"/>	<input type="checkbox"/>
(Day/Month/Year Field) (出願年月日)	Yes はい	No いいえ
_____	<input type="checkbox"/>	<input type="checkbox"/>
(Day/Month/Year Field) (出願年月日)	Yes はい	No いいえ

I hereby claim the benefit under Title 35, United States Code, Section 119 (e) of any United States provisional application(s) listed below.

<u>_____</u>
(Status: Patented, Pending, Abandoned) (現況：特許許可済み、係属中、放棄済)

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s), or Section 365 of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of Title 35, United States Code Section 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of application.

<u>_____</u>
(Status: Patented, Pending, Abandoned) (現況：特許許可済み、係属中、放棄済)

<u>_____</u>
(Status: Patented, Pending, Abandoned) (現況：特許許可済み、係属中、放棄済)

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Japanese Language Declaration

(日本語宣告書)

委任状：私は下記の発明者として、本出願に関する一切の手続きを米国特許商標局に対して遂行する弁理士または代理人として、下記の者を指名いたします。
(弁理士、または代理人の氏名及び登録番号を明記のこと)

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Japanese Language Declaration

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